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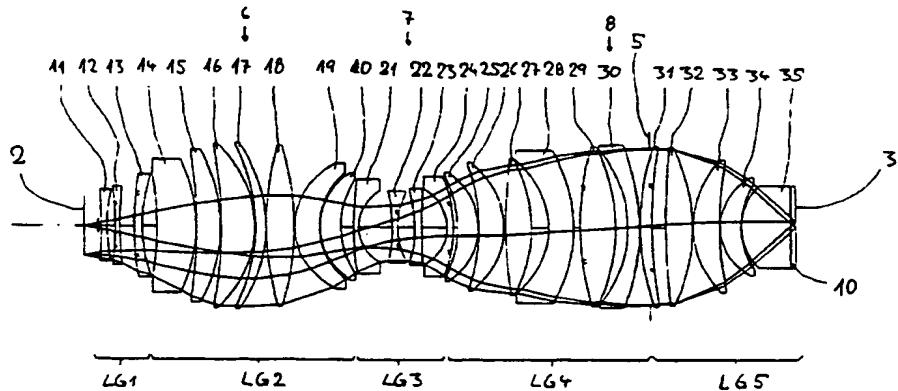
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(54) Title: REFRACTIVE PROJECTION OBJECTIVE FOR IMMERSION LITHOGRAPHY



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(57) Abstract: A purely refractive projection objective suitable for immersion microlithography is designed as a single-waist system with five lens groups, in the case of which a first lens group with a negative refracting power, a second lens group with a positive refracting power, a third lens group with a negative refracting power, a fourth lens group with a positive refracting power and a fifth lens group with a positive refracting power are provided. The system aperture is in the region of maximum beam diameter between the fourth and the fifth lens group. Embodiments of projection objectives according to the invention achieve a very high numerical aperture of $NA > 1$ in conjunction with a large image field, and are distinguished by a good optical correction state and moderate overall size. Pattern widths substantially below 100 nm can be resolved when immersion fluids are used between the projection objective and substrate in the case of operating wavelengths below 200 nm.



For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

Description

Refractive projection objective for immersion lithography

The invention relates to a refractive projection objective for projecting a pattern arranged in an object plane of the projection objective into an image plane of the projection objective with the aid of an immersion medium which is arranged between a last optical element of the projection objective and the image plane.

Photolithographic projection objectives have been in use for several decades for producing semiconductor components and other finely structured structural elements. They serve the purpose of projecting patterns of photomasks or reticles, which are also denoted below as masks or reticles, onto an object coated with a photosensitive layer with very high resolution on a reducing scale.

Three developments running in parallel chiefly contribute to the production of every finer structures of the order of magnitude of 100 nm or below. Firstly, an attempt is being made to increase the image-side numerical aperture (NA) of the projection objective beyond the currently customary values into the region of NA=0.8 or above. Secondly, ever shorter wavelengths of ultraviolet light are being used, preferably wavelengths of less than 260 nm, for example 248 nm, 193 nm, 157 nm or below. Finally, still other measures are being used to increase resolution, for example phase-shifting masks and/or oblique illumination.

In addition, there are already approaches to improving the achievable resolution by introducing an immersion medium of high refractive index into the space between the last optical element of the projection objective and the substrate. This technique is denoted here as immersion lithography. Introducing the immersion medium yields an effective wavelength of

$$\lambda_{\text{eff}} = \lambda_0/n,$$

λ_0 being the vacuum operating wavelength and n the refractive index of the immersion medium. This yields a resolution of

5

$$R = k_1 (\lambda_{\text{eff}}/NA_0)$$

and a depth of focus (DOF) of

10

$$\text{DOF} = \pm k_2 (\lambda_{\text{eff}}/NA_0^2),$$

$NA_0 = \sin \Theta_0$ being the "dry" numerical aperture, and Θ_0 being half the aperture angle of the objective. The empirical constants k_1 and k_2 depend on the process.

15

The theoretical advantages of immersion lithography reside in the reduction of the effective operating wavelength and the resolution improved thereby. This can be achieved in conjunction with an unchanged vacuum wavelength, and so established techniques for 20 producing light for selecting optical materials, for coating technology etc. can be adopted largely without change for the appropriate wavelength. However, measures are required for providing projection objectives with very high numerical apertures in the region of $NA = 1$ or above. Furthermore, suitable immersion media must be available.

25

The article entitled "Immersion Lithography at 157 nm" by M. Switkes and M. Rothschild, J. Vac. Sci. Technol. Vol. 19 (6), Nov./Dec. 2001, pages 1 ff. presents immersion fluids based on perfluoropolyethers (PFPE) which are sufficiently transparent for a working wavelength of 30 157 nm and are compatible with some photoresist materials currently being used in microlithography. One tested immersion fluid has a

refractive index of $n = 1.37$ at 157 nm. The publication also describes a lens-free optical system, operating with calcium fluoride elements and silicon mirrors, for immersion interference lithography, which is intended to permit the projection of 60 nm structures and below in conjunction

5 with a numerical aperture of $NA = 0.86$. The optical system may not be suitable for use in the series production of semiconductors or the like.

Patent Specification US 5,610,683 (corresponding to EP 0 605 103) describes a projection exposure machine, provided for immersion

10 lithography, having devices for introducing immersion fluid between the projection objective and the substrate. No design is specified for the optical projection system.

US Patent US 5,900,354 proposes using a super-critical fluid, for

15 example xenon gas, as immersion medium in immersion lithography. No design is shown for a suitable projection objective.

It is the object of the invention to create a refractive projection objective which is suitable for immersion lithography and which has, in conjunction

20 with a moderate overall size, a high numerical aperture suitable for immersion lithography, an image field which is sufficiently large for practical use in wafer steppers or wafer scanners, and a good correction state.

25 This object is achieved by means of a projection objective having the features of Claim 1. Advantageous embodiments are specified in the dependent claims. The wording of all the claims is incorporated in the description by reference.

30 In accordance with one aspect of the invention, a refractive projection objective for projecting a pattern arranged in an object plane of the projection objective into the image plane of the projection objective with

the aid of an immersion medium which is arranged between a last optical element of the projection objective and the image plane has a first lens group, following the image plane, with a negative refracting power;

5 a second lens group, following thereupon, with a positive refracting power;

a third lens group, following thereupon, with a negative refracting power;

a fourth lens group, following thereupon, with a positive refracting power;

a fifth lens group, following thereupon, with a positive refracting power;

10 and

a system aperture which is arranged in the region of maximum beam diameter between the fourth lens group and the fifth lens group.

This refracting power distribution produces a projection objective having

15 two bellies and a waist therebetween, a good correction of the field curvature thereby being achieved. The system aperture is seated in the region of greatest beam diameter of the belly next to the image plane, preferably at least 90% or 95% of the maximum beam diameter being present in the belly near the image at the location of the system

20 aperture. In certain embodiments, the system aperture can lie between a plane of maximum beam diameter near the image and the image plane, and thus in a region in which the transilluminated diameter of the objective already decreases towards the image plane. This is a substantial difference from conventional, refractive projection objectives

25 in which the system aperture lies on the object side at a relatively large distance in front of the region of maximum beam diameter in the belly near the image.

The design permits image-side numerical apertures $NA \geq 0.9$, it being

30 possible in the case of preferred embodiments to achieve $NA = 1.1$ or above. Preferred projection objectives are adapted to an immersion liquid which has a refractive index of $n > 1.3$ at the operating wavelength. As a

result, a reduction in the effective operating wavelength by 30% or more can be achieved by a comparison with systems without immersion.

The projection objective can advantageously be designed such that the

5 space to be filled up by the immersion medium has an axial thickness which is so small that transmission losses in the immersion medium are no more than 10 to 20% of the penetrating light intensity. Consequently, image-side working distances of less than 200 μm , in particular less than 100 μm , are favourable. Since, on the other hand, touch contact

10 between the last optical element and the substrate surface is to be avoided, a lower limit for the working distance of from 10 to 20 μm should not be undershot. Larger working distances in the region of one or more millimeters are also possible given suitably transparent immersion media.

15 Preferred projection objectives are distinguished by a number of favourable structural and optical features which are necessary alone or in combination for the suitability of the objective as an immersion objective.

20 For example, it can be favourable when the refracting powers of the lens groups are of the same order of magnitude on both sides of the system aperture. In particular, it can be provided that a ratio between the focal length of the fourth lens group and the focal length of the fifth lens group

25 is between approximately 0.9 and approximately 1.1. It can likewise be favourable when the focal lengths or refracting powers of the lens groups near the object and lens groups near the image are similar in magnitude. In particular, a ratio of the magnitudes of the focal lengths of the first lens group and the fifth lens group can be between

30 approximately 0.7 and approximately 1.3, preferably between approximately 0.9 and 1.1. Furthermore, it can be favourable for

producing a high image-side numerical aperture when a strong positive refracting power is concentrated in the region near the image. In preferred embodiments, a ratio between the overall length of the projection objective and the focal length of the fifth lens group following 5 the system aperture is greater than five, in particular greater than six, seven or even eight. The axial distance between the object plane and image plane is denoted here as overall length.

In order to achieve a good correction state, it is provided in preferred 10 embodiments that the first lens group includes at least one aspheric surface. Favourably, it is even possible for a plurality of aspherics, for example two, to be provided here. Aspherics in this region make a particularly effective contribution to the correction of distortion and astigmatism. It is favourable, furthermore, for the correction of coma and 15 astigmatism when the third lens group, situated in the region of the waist, has at least one aspheric surface, a plurality of aspherics, for example two aspherics, being preferred. In the case of preferred embodiments, at least one aspheric is provided in each lens group in order to facilitate fine setting of the correction state of the projection 20 objective. With regard to simple production of the lenses, the number of aspherics should be limited, for example to less than nine or less than seven, as in the case of a preferred embodiment.

The favourable projection properties of projection objectives according to 25 the invention, particularly the good correction state in the case of a very high numerical aperture, are promoted by some special features relating to the type and arrangement of the lenses used. For example, it is favourable when at least one meniscus lens, convex relative to the object plane, with a negative refracting power is arranged in the near 30 zone of the object plane, in particular in the first lens group. This lens, which can form the third lens of the objective, for example, favours the correction of tangential astigmatism.

The second lens group preferably has at least one, in particular a plurality of meniscus lenses, concave relative to the object plane, with a positive refracting power on its side facing the object plane. These preferably combine with at least one, preferably a plurality of meniscus

5 lenses, convex relative to the object plane, with a positive refracting power on the side, facing the image plane, of the second lens group. At least one biconcave positive lens is favourably situated between the menisci or meniscus groups of the opposing bending. As a result, a sequence of at least one positive meniscus lens, concave relative to the

10 object plane, a biconvex positive lens and at least one positive meniscus lens, concave relative to the image plane, can be formed in the second lens group. This sequence of lenses in the region of relatively large beam diameter of the first belly is favourable for a strong "deformation" of the main ray in this region in conjunction with low areal stresses of the

15 optical surfaces. This is favourable for low total aberrations of the projection objective. A favourable areal stress in the sense of this application occurs whenever the incidence angles of the rays striking an optical surface are as small as possible and do not overshoot a critical limit value. Denoted here as incidence angle is the angle between the

20 impingement direction of a ray on an optical surface and the surface normal of the optical surface at the impingement point of the ray. The smaller the incidence angle and, correspondingly, the lower the areal stress, the easier is the development of suitable antireflection coatings, and the greater is the tolerance of the design to the adjustment.

25 The region of narrowest constriction of the ray is denoted as the waist. The third lens group in the region of the waist has the task of re-expanding the radiation, converging downstream of the first belly, with as few aberrations as possible. It is favourable for this purpose when the

30 third lens group has only lenses with a negative refracting power. It has proved to be particularly advantageous when, with reference to a plane of symmetry lying inside the third lens group, the third lens group is of

substantially symmetrical construction. This is distinguished, in particular, by virtue of the fact that mutually assigned lenses of the same type are arranged on the object side and image side of the plane of symmetry. The symmetry of the lens types preferably also extends into

5 the bordering region of the second and fourth lens groups such that an exit region, facing the third lens group, of the second lens group, and an entry region, following the third lens group, of the fourth lens group can be constructed substantially symmetrically relative to the plane of symmetry lying inside the third lens group. A symmetrical arrangement

10 of negative and positive meniscus lenses will be explained in further detail in conjunction with the embodiments. The symmetry promotes a low areal stress of the lenses in conjunction with few aberrations.

At least one doublet with a biconvex positive lens and a meniscus-shaped negative lens, following towards the image, with lens surfaces which are concave towards the object is preferably provided in the region directly upstream of the system aperture, that is to say in the fourth lens group. Particularly favourable are embodiments having two such doublets which can follow one another directly. A positive air lens,

20 convex relative to the image plane, is respectively arranged between the lenses of the doublet. Such doublets composed of a collecting biconvex lens and a diverging meniscus have a positive effect on the correction state and can counteract the aberrations which are introduced by lenses with a strong, positive diffracting power downstream of the system aperture. It can be favourable, moreover, to arrange in the object-side entry region of the fourth lens group at least one meniscus lens, concave towards the object, with a positive refracting power, in order to collect the radiation coming from the waist in conjunction with a low areal stress.

25

30 In order to achieve very high numerical apertures, it is advantageous when the fifth lens group has exclusively positive lenses. It is possible,

for example, to arrange four or more positive lenses between aperture stop and image plane. In this case, favourable surface loads can be achieved whenever at least one meniscus lens, concave towards the image, with a positive refracting power is provided in the fifth lens group.

- 5 In particular, two or more such lenses can be provided. The last optical element is preferably formed by a plano-convex lens which preferably has a spherical entry surface and a substantially flat exit surface. It is possible thereby, on the one hand, to achieve a good correction of spherical aberration and coma and, on the other hand, a substantially flat exit surface is favourable for immersion lithography. In preferred embodiments, the plano-convex lens is nonhemispherical, the centre of the spherical surface lying outside the lens. Truncated hemispherical lenses of this type can yield a reduced sensitivity to fluctuations in the working distance.

- 15 By applying some or all of these design principles, success has been achieved in preferred embodiments which keep the surface loads of the lenses so low that despite an aperture of more than $NA = 0.9$ or 1, incidence angles whose sine is greater than approximately 90% or even 20 approximately 85% of the image-side numerical aperture do not occur at any of the optical surfaces, and this simplifies the coating of the lenses and the adjustment of the objective.

- 25 In preferred embodiments, all the lenses of the projection objective consist of the same material. For operating wavelengths of 193 nm, synthetic quartz glass and, for operating wavelengths of 157 nm, calcium fluoride can be used, for example, as material. The use of only one kind of material facilitates production and permits simple adaptation of the objective design to other wavelengths. It is also possible to 30 combine a plurality of kinds of material in order, for example, to support the correction of chromatic aberrations. It is also possible to use other UV-transparent materials such as BaF_2 , NaF , LiF , SrF , MgF_2 or the like.

In addition to the claims, the description and the drawings also disclose the preceding and further features, it being possible for the individual features to be implemented on their own or severally in the form of subcombinations in the case of embodiments of the invention and in 5 other fields, and for them to constitute advantageous designs which can be protected per se. In the drawings:

10 Figure 1 shows a lens section through a first embodiment of a refractive projection objective which is designed for a 193 nm operating wavelength;

15 Figure 2 shows a lens section through a second embodiment of a projection objective which is designed for a 193 nm operating wavelength;

20 Figure 3 shows a lens section through a third embodiment of a projection objective which is designed for a 157 nm operating wavelength; and

25 Figure 4 shows a lens section through a fourth embodiment of a projection objective which is designed for a 193 nm operating wavelength.

In the following description of preferred embodiments, the term "optical axis" denotes a straight line through the centres of curvature of the 25 optical components. Directions and distances are described as on the image side or towards the image when they are aligned in the direction of the image plane or the substrate, which is to be exposed, located there, and as on the object side or towards the object when they are 30 directed towards the object with reference to the optical axis. In the examples, the object is a mask (reticle) with the pattern of an integrated circuit, but it can also be another pattern, for example a grating. In the

examples, the image is formed on a wafer which serves as a substrate and is provided with a photoresist layer, but other substrates are also possible for example elements for liquid crystal displays or substrates for optical gratings. The focal lengths specified are focal lengths with

5 reference to air.

Identical or mutually corresponding features of the various embodiments are denoted below with the same reference symbols for reasons of clarity.

10 A typical design of an embodiment of a purely refractive reduction objective 1 according to the invention is shown with the aid of Figure 1. It serves the purpose of projecting in conjunction with virtually homogeneous immersion a pattern, arranged in an object plane 2, of a

15 reticle or the like into an image plane 3 to a reduced scale, for example to the scale of 5:1. This is a rotationally symmetrical single-waist system with five lens groups which are arranged along the optical axis 4, which is perpendicular to the object plane and image plane, and form an object-side belly 6, an image-side belly 8 and a waist 7 situated

20 therebetween. The first lens group LG1, following the image plane 2, has a negative refracting power and a focal length of -166 mm. A second lens group LG2, following thereupon, has a positive refracting power with a focal length of 121 mm. A third lens group LG3, following thereupon, has a negative refracting power and a focal length of -

25 33 mm. A fourth lens group LG4, following thereupon, has a positive refracting power with a focal length of 166 mm, which therefore corresponds in terms of magnitude to the focal length of the first lens group. A fifth lens group LG5, following thereupon, has a positive refracting power and a focal length of 170 mm, which is of the order of

30 magnitude of the focal length of the fourth lens group and of the first lens group LG1 in terms of magnitude. The system aperture 5 is arranged between the fourth lens group LG4 and the fifth lens group LG5 in the

region, near the image, of maximum beam diameter, that is to say in the second belly 8 of the objective.

The first lens group LG1, following the object plane 2, is substantially responsible for the expansion of the light bundle into the first belly 6. It

- 5 comprises three lenses 11, 12, 13 with a negative refracting power, the first lens 11 and the second lens 12 being configured as biconvex negative lenses. The third lens 13 is a diverging meniscus in the case of which as a special feature the concave side is directed not towards the object 2 but towards the image plane 3. This arrangement is very
- 10 favourable for correcting the tangential astigmatism. Otherwise, the first lens group includes two aspherics, specifically the entry sides of the second and the third lens. The aspherics have a positive influence on the very good correction of the distortion and the astigmatism.
- 15 The second lens group LG2 comprises four collecting menisci 14, 15, 16, 17, facing the reticle or the object plane 2 with their concave side, a biconvex positive lens 18 and two collecting menisci 19, 20 facing the wafer or the image plane 3 with their concave side. This design, in which the curvatures of the meniscus surfaces run on the object side and
- 20 image side of the biconvex lens 18 in opposite directions with concave surfaces averted from one another, ensures small areal stresses for the menisci and the positive lens 18, and thus few aberrations. The biconcave air lens between the biconvex positive lens 18 and the following meniscus lens 19 has with its strong astigmatic undercorrection
- 25 a favourable influence on the balancing-out of the astigmatism in the front part of the system upstream of the waist 7.

The third lens group LG3 consists exclusively of diverging lenses, specifically a negative meniscus lens 21 with image-side concave

- 30 surfaces, a biconcave negative lens 22, following thereupon, a further biconcave negative lens, following thereupon, and a negative meniscus lens 24, following thereupon, with object-side concave surfaces. With

reference to a plane of symmetry 9 lying between the lenses 22 and 23, these four lenses are designed with mirror symmetry with regard to lens type (meniscus lens or biconcave lens) and direction of curvature of the optical surfaces. Together with the last two lenses 19, 20 of the second 5 lens group and the first two lenses 25, 26 of the fourth lens group LG4, following thereupon, there is a series of two collecting menisci 19, 20 and one diverging meniscus 21, all three of which have concave surfaces facing the waist or the plane of symmetry 9. In the opposite, mirrored direction, that is to say on the image side of the plane of 10 symmetry 9, the two biconcave negative lenses 22, 23 are again followed at the waist, that is to say in the area of smallest diameter, by a diverging meniscus 24 and two collecting menisci 25, 26 of the fourth lens group. This design having mirror symmetry relative to the plane of symmetry 9 supports a low tensioning or a low areal stress of the optical 15 surfaces, and thus few aberrations.

The third lens group includes, in the form of the exit surface of the smallest lens 22 and the exit surface of the negative meniscus lens 24, two aspherics which make a substantial contribution to the correction of 20 the coma and the astigmatism.

The fourth lens group LG4 comprises on its entry side two positive meniscus lenses 25, 26 which are concave relative to the object plane and are followed by two doublets 27, 28 and 29, 30. Each of the 25 doublets has, on the object side, a collecting biconvex lens 27 and 29, respectively, and downstream thereof a diverging meniscus 28 and 30, respectively, whose concave surfaces point towards the object plane. The two spherically strongly overcorrected, diverging menisci 28 ($f = -728$ mm) and 30 ($f = -981$ mm) counteract the strongly undercorrected, 30 collecting lenses of the fifth lens group LG5 following downstream of the system aperture 5. The combination of the collecting biconvex lens and the diverging meniscus inside a doublet has a very positive effect on the

correction of image errors in the region of the second belly 8. With their strong overcorrection of the tangential astigmatism, the two menisci 28, 30, in particular the thick meniscus 28, counteract the undercorrection in the fifth lens group LG5.

5

The fifth lens group LG5, situated downstream of the system aperture 5, is substantially responsible for producing the high numerical aperture.

Provided for this purpose are exclusively collecting lenses, specifically a positive meniscus lens 31, arranged in the region of the system aperture

10 5, with surfaces concave towards the image, a biconvex positive lens 32, following thereupon, with a slightly curved entry side and a more strongly curved exit side, a positive meniscus lens 23, following thereupon, with surfaces concave towards the image, a further positive meniscus lens 24, likewise with surfaces concave towards the image, and a terminating 15 plano-convex lens 35 with a spherical entry side and a flat exit side. The positive lenses 31, 32, 33 and 34 are strongly undercorrected spherically and overcorrected with reference to the coma. In the case of this design, the correction of the spherical aberration and the coma is therefore implemented substantially in conjunction with the configuration of the 20 fourth lens group LG4 which is situated upstream of the system aperture 5 and creates a corresponding offset of these aberrations.

Consequently, the fourth lens group LG4 and the fifth lens group LG5 are responsible in combination for achieving a good correction state of 25 the spherical aberration and of coma. An aspheric surface on the entry side of the biconvex lens 27 of the first doublet substantially supports the correction of the spherical aberration, but also of the coma of third order. An aspheric surface, arranged in the vicinity of the system aperture 5, on the exit side of the positive meniscus lens 31, convex towards the object, 30 at the input of the fifth lens group LG5 chiefly corrects aberrations of higher order and thereby makes a substantial contribution to setting a good aberration compromise. A likewise positive influence on the

correction of aperture aberration and coma is exerted by the spherical, convex entry surface of the plano-convex lens 35. The latter is spherically overcorrected and undercorrected with reference to coma.

- 5 The system has a working distance on the image side of approximately 8.4 mm, which can be filled up by an immersion fluid 10. Deionized water (refractive index $n = 1.47$) or another suitable transparent liquid, for example, can be used at 193 nm as immersion fluid.
- 10 The correction state of the optical system 1 is excellent. All aberrations are corrected. The RMS value of the wavefront deformation is very low at $4 \text{ m}\lambda$. The distortion of all field points in the region is below 1 nm. A projection objective is thus created which operates at an operating wavelength of 193 nm, can be produced with the aid of conventional
- 15 techniques for lens production and coating, and permits a resolution of structures substantially below 100 nm.

The design described is fundamentally suitable for near-field lithography, as well, by the use of a homogeneous immersion. For this purpose, the

- 20 terminating plano-convex lens 35 is to be combined with the immersion layer 10 to form a lens which can consist, for example, of synthetic quartz glass. In order to permit sufficient light energy of the evanescent field to be coupled in, in this case the working distance between the exit surface of the projection objective and the image plane should be in the
- 25 region of 100 nm or below.

The specification of the design is summarized in a known way in tabular form in Table 1. Here, column 1 gives the number of a refracting surface, or one distinguished in another way, column 2 gives the radius r of the

- 30 surface (in mm), column 3 gives the distance d denoted as thickness, of the surface from the following surface (in mm), column 4 gives the material of the optical components, and column 5 gives the refractive

index of the material of the component, which follows the entry surface. The useful, free radii or half the free diameter of the lenses (in mm) are specified in column 6.

- 5 In the case of the embodiment, six of the surfaces, specifically the surfaces 4, 6, 15, 29, 34 and 44, are aspheric. Table 2 specifies the corresponding aspheric data, the aspheric surfaces being calculated using the following rule:
- 10 $p(h) = [((1/r)h^2)/(1+SQRT(1-(1+K)(1/r)^2h^2))] + C1 \cdot h^4 + C2 \cdot h^6 + \dots$

Here, the reciprocal (1/r) of the radius specifies the surface curvature, and h the distance of a surface point from the optical axis.

Consequently, p(h) gives the so-called sagitta, that is to say the distance 15 of the surface point from the surface apex in the z direction, that is to say in the direction of the optical axis. The constants K, C1, C2, ... are reproduced in Table 2.

The optical system 1, which can be reproduced with the aid of these 20 data, is designed for an operating wavelength of approximately 193 nm, for which the synthetic quartz glass used for all the lenses has a refractive index $n = 1.56029$. The image-side numerical aperture is 1.1. The system is adapted to a refractive index of the immersion medium 10 of $n = 1.56$, which permits a virtually ideal coupling of the light into the 25 immersion layer 10. The objective has an overall length (distance between image plane and object plane) of 1162 mm. A light conductance (product of numerical aperture and image size, also denoted étendue or geometrical flux) of 24.1 mm is achieved given an image size of 22 mm.

30 A variant of the projection objective shown in Figure 1 is explained with the aid of Figure 2. Lenses or lens groups of the same type or the same

function are denoted by the same reference symbols for reasons of clarity. The system 1' is optimized for a refractive index of the immersion medium of $n = 1.37$, and this corresponds to a value, which has become known from the literature, of 157 nm for the refractive index of an 5 immersion fluid based on perfluoropolyether (PFPE).

The fourth and the fifth lens group differ in terms of design from that in accordance with Figure 1. In LG4, the thick meniscus lens 28 of the first doublet in Figure 1 is split up into an object-side, biconcave negative 10 lens 28' with an only slightly curved exit side and a subsequent biconvex positive lens 28" with a correspondingly only slightly curved entry side. This splitting-up further reduces the areal stress of the optical surfaces in this region. The rim ray of the projection runs in a converging fashion in the air space between the subsequent lenses 29, 30 upstream of the 15 entry surface of the meniscus 30 which is concave towards the object. In the fifth lens group LG5, the entry-side lenses 31, 32, separated in the case of the design in Figure 1 and downstream of the system aperture 5 are combined to form a single, biconvex positive lens 32'. This is situated at a distance downstream of the system aperture 5, which can 20 be accessed particularly easily. A further special feature consists in that the system aperture 5 is situated between a plane, near the image, of maximum beam diameter and the image plane 3, that is to say where the transilluminated diameter of the lenses already decreases towards the image plane. The other lenses correspond with regard to the type 25 and sequence of the lenses of identical reference symbols in Figure 1. In the case of this design, as well, all the lenses consist of synthetic quartz glass. The specification of this design in the notation described is specified in Tables 3 and 4.

30 Shown in Figure 3 is a third embodiment, designed for an operating wavelength of 157 nm, of a projection objective 1" whose specification is given in Tables 5 and 6. It is to be seen from the sequence and the type

of lenses that the design is based on the design principle explained with the aid of Figures 1 and 2, and so the same reference symbols are used for lenses and lens groups with corresponding functions. As in the case of the embodiment in accordance with Figure 1, no further optical

5 element is arranged upstream of the first biconcave negative lenses 11 of the objective. As in the case of the embodiment in accordance with Figure 2, in the fourth lens group LG4 the thick meniscus lens 28, still in one piece in Figure 1, is split up into a biconcave negative lens 28' and a directly following biconvex positive lens 28''. Just as in the case of the

10 embodiment in accordance with Figure 2, the function of the entry-side lenses 31, 32 of the embodiment in accordance with Figure 1 is taken over by a single, biconvex positive lens 32' which initiates the ray combination towards the image plane. In a way similar to the case of the embodiment in accordance with Figure 2, the system aperture 5 is

15 situated inside the second belly 8 downstream of the region of maximum beam diameter, that is to say where the beam diameter already decreases again towards the image plane.

20 The refractive index for the immersion medium is set at $n = 1.37$, which corresponds to a value, which has become known from the literature, for a PFPE-based immersion fluid sufficiently transparent at 157 nm. The image-side working distance is set to approximately 50 μm , which corresponds in practical use to the thickness of the immersion layer. It may be assumed that suitable immersion fluids still have high

25 transmission values of more than 90% in the case of this low thickness, and so only negligible, low transmission losses occur in the region of the immersion, this being favourable for achieving a satisfactory wafer throughput. Pattern widths of less than 70 nm can be resolved with the aid of this purely refractive projection objective, of excellent correction

30 state, which can be implemented using conventional means.

Tables 7 and 8 show the specification of an embodiment (not illustrated pictorially) of a projection objective which is derived from the embodiment in accordance with Figure 3, from which it differs essentially in that the thick meniscus lens 17, concave towards the object, there is

5 replaced by a thinner meniscus lens curved in the same direction. A comparison of Tables 5 and 6 shows that as a result an even more compact design is possible which has smaller lens diameters and a smaller overall length in conjunction with equally good optical properties.

10 A fourth embodiment of a projection objective 1'', which is designed for an operating wavelength of 193 nm and whose specification is given in Tables 9 and 10 is shown in Figure 4. This embodiment has a projection scale of 4:1 and an image-side numerical aperture $NA = 0.9$. A comparison with the remaining embodiments shows that less lens

15 material is required in conjunction with the same fundamental optical principle. Instead of 25, as in the case of the other embodiments, there is a need for only 23 lenses, and moreover the average and maximum lens diameters are smaller than with the preceding embodiments. In particular, there is provision in the second lens group LG2 for only three

20 menisci 14, 15, 16, concave towards the object, a lens corresponding to the menisci 17 of the other embodiments being absent. In contrast to the other embodiments, in the fourth lens group LG4 only one doublet 27 and 28 is provided, and so a saving of one lens is made in this lens group as well. The symmetrical design of the third lens group LG3 and of

25 the lens pairs bordering thereon, 19, 20, of the second lens group and 25, 26 of the fourth lens group corresponds to that of the other embodiments. The embodiment in accordance with Figure 4 substantiates that it is also possible to implement solutions of favourable design within the scope of the invention for relatively large projection

30 scales and relatively large fields.

The correction state of all the embodiments shown is excellent. All aberrations are corrected. The maximum RMS value of the wavefront deformation is very low and is below $4.5 \text{ m}\lambda$ for the embodiments in accordance with Figures 1 and 2, below $6.5 \text{ m}\lambda$ for the embodiment in accordance with Tables 7 and 8, and below $5.2 \text{ m}\lambda$ for the embodiment in accordance with Figure 4. Within all the systems, the distortion is in the region below 1 nm for all field points.

It can be seen by the person skilled in the art from the examples that numerous modifications of the designs are possible within the scope of the invention. For example, individual lenses can be split up into two or more separate lenses, or separate lenses can be combined to form a single lens having essentially the same function.

Embodiments with two or more lens materials are also possible. For example, in the case of embodiments for 193 nm it is possible to provide a combination of lenses made from synthetic quartz glass and calcium fluoride in order to facilitate chromatic correction and in order to avoid changes in refractive index because of compaction in regions of high radiation energy densities by using calcium fluoride lenses. Also possible is the use of other materials transparent to the ultraviolet light used, such as barium fluoride, sodium fluoride, lithium fluoride, strontium fluoride, magnesium fluoride or the like.

Catadioptric systems for immersion lithography can also be designed using essential configuration features of the embodiments represented here, in particular in the region, near the image, of the second belly and the aperture stop.

The technical teaching of the invention explained with the aid of various exemplary embodiments shows that a range of design boundary

conditions should be taken into account when the aim is to design an optical system suitable for immersion lithography, particularly one of such compact design. The following features can be beneficial individually or in combination. Immersion objectives for which the image

5 field diameter is greater than approximately 1%, in particular greater than approximately 1.5% of the overall length are favourable. Favourable light conductances (product of image field diameter and numerical aperture) are in the region of above 1%, in particular above 2% of the overall length. Four or more collecting lenses between

10 aperture stop and image plane are favourable, it being preferred for only collecting lenses to be provided in this region. Preferably more than four, five or six consecutive collecting lenses are favourable in the second lens group. In this case, preferably two or more collecting menisci with an object-side concave surface are favourable in the entry region of the

15 second lens group, and two or more collecting menisci with surfaces concave towards the image are favourable at the end of the second lens group. In the region of the first belly or of the second lens group a strong beam expansion is beneficial for which the maximum beam diameter is preferably more than 1.8 times, in particular more than 2 times the object

20 field diameter. The maximum lens diameter in the second lens group can be approximately twice the minimum free lens diameter of the third lens group in the region of the constriction. The maximum lens diameter in the second belly following the constriction is preferably of the same order of magnitude and can, in particular, be greater than twice the

25 minimum free diameter in the third lens group. In the region of the third lens group, that is to say in the region of the waist of the system, two concave surfaces are preferably directly opposite one another and are enclosed by two surfaces curved in the same sense. The lenses respectively adjoining towards the object and towards the image are also

30 preferably designed and arranged in this way.

Particular lens distributions can be favourable. In particular, it is favourable when substantially more lenses are situated upstream of the system aperture than downstream of the aperture. The number of lenses upstream of the aperture is preferably at least four times, in particular

- 5 more than five times, the number of lenses downstream of the system aperture. Five or more collecting lenses are preferably arranged between the region of narrowest constriction and the system aperture or aperture stop; the axial distance between the region of narrowest constriction and the aperture stop arranged exceptionally near the image
- 10 is favourably at least 26%, if appropriate more than 30% or 35%, of the overall length of the projection objectives.

Further special features relate to the trajectory of and the relationships between principal rays and rim rays of the projection. Denoted here as

- 15 principal ray is a ray which runs from a rim point of the object field parallel or at an acute angle to the optical axis and which cuts the optical axis in the region of the system aperture. A rim ray in the sense of the present application leads from the middle of the object field to the rim of the aperture stop. The perpendicular distance of these rays from the
- 20 optical axis yields the corresponding ray height. It can be favourable when the principle ray height is greater in absolute value up to the end of the second lens group than the rim ray height, this relationship preferably not being reversed until in the region of the third lens group. The maximum rim ray height is preferably more than twice, in particular
- 25 more than 2.3 to 2.5 times, the rim ray height in the region of the narrowest constriction of the third lens group. It is favourable when the diameter of the rim ray is kept small in the region between the fourth and fifth lens groups, that is to say in the region of the system aperture. This corresponds to a smallest possible focal length of the fifth lens group,
- 30 following the system aperture. The focal length of the fifth lens group is preferably smaller than 15%, in particular smaller than 10% of the overall length. Preferred systems are doubly telecentric, and so the principal ray

is substantially perpendicular both to the object plane and to the image plane. In preferred systems, the principal ray coming from the object field should still have a divergent trajectory after at least five lenses, that is to say a trajectory with a still rising principal ray height away from the 5 optical axis. It is favourable, furthermore, when the sine of the maximum principal ray divergence angle in the objective region near the object is more than 50% of the object-side numerical aperture. A plurality of aspheric surfaces are preferably provided in the region near the object in which the rim ray height is greater than the principal ray height, in order 10 to promote a favourable correction state.

The invention also relates to a projection exposure machine for microlithography which is distinguished in that it includes a refractive projection objective in accordance with the invention. The projection 15 exposure machine preferably also has devices intended for introducing and keeping an immersion medium, for example a liquid of suitable refractive index, between the last optical surface of the projection objective and the substrate to be exposed. Also covered is a method for producing semiconductor components and other finely structured 20 structural elements, in the case of which an image of a pattern arranged in the object plane of a projection objective is projected in the region of the image plane, an immersion medium arranged between the projection objective and the substrate to be exposed and transparent to light at the operating wavelength being transilluminated.

Table 1

SURFACE	RADIUS	THICKNESSES	LENSES	REFRACTIVE INDEX		1/2 FREE DIAMETER
				193.304 nm	193.304 nm	
0	0.000000000	21.660160000				55.000
1	0.000000000	5.665665462				59.973
2	-697.373131352	6.6307388015	SIO2	1.56028900		60.658
3	317.877790816	12.366856184				63.806
4	-385.517361474AS	6.616967568	SIO2	1.56028900		65.103
5	684.578717634	23.692566944				70.051
6	612.57904180GAS	13.565639007	SIO2	1.56028900		66.338
7	315.238108546	24.650771766				92.585
8	-636.903175512	64.776662854	SIO2	1.56028900		95.153
9	-204.036729565	1.004000000				120.585
10	-942.407223581	39.155776761	SIO2	1.56028900		130.798
11	-317.623154272	1.312033169				137.817
12	-856.579360710	53.655176362	SIO2	1.56028900		145.587
13	-222.120764338	1.000000000				148.413
14	-365.979641333	16.565547178	SIO2	1.56028900		148.696
15	-300.375347712	1.000000000				150.000
16	622.472470310	44.751302453	SIO2	1.56028900		146.385
17	-556.306013695	1.620913522				145.384
18	135.290972565	40.672419816	SIO2	1.56028900		113.552
19	140.238400611	1.607703555				99.382
20	128.146489274	33.605630320	SIO2	1.56028900		97.047
21	178.381821741	21.317336106				87.913
22	764.210626300	0.040530767	SIO2	1.56028900		65.346
23	81.619567541	55.131180427				66.098
24	-324.577506735	6.010204876	SIO2	1.56028900		63.499
25	133.065440504AS	29.11G630876				62.507
26	-275.984572757	12.121405585	SIO2	1.56028900		63.961
27	2605.503343355	41.843073620				68.171
28	-83.024363434	9.3166662930	SIO2	1.56028900		69.398
29	-271.500670516AS	7.122879020				90.369
30	-234.062816820	34.813633191	SIO2	1.56028900		93.111
31	-128.679213398	1.375380851				98.648
32	-371.070689222	40.564766288	SIO2	1.56028900		112.720
33	-158.555144143	2.142646331				116.032
34	844.565103125AS	42.656894676	SIO2	1.56028900		123.022
35	-293.770426726	26.164527693				122.344
36	-170.081620687	40.277028630	SIC2	1.56028900		122.713
37	-316.315520485	10.9436C7028				137.139
38	623.625571533	56.798798905	SIO2	1.56028900		143.361
39	-175.372716473	20.156323351				143.119
40	-246.931005408	18.567257168	SIO2	1.56028900		142.262
41	-460.148730828	16.4e5394474				145.978
42	0.000000000	-15.4e5394474				144.329
43	506.966830874	18.675460556	SIO2	1.56028900		144.915
44	1011.956468931AS	22.930981004				144.124
45	1760.7C1259607	42.719861927	SIC2	1.56028900		143.914
46	-371.926449461	1.351397272				143.620
47	194.244261562	42.532993241	SIC2	1.56028900		120.019
48	689.962205932	1.126753967				114.527
49	109.590774593	34.370356665	SIO2	1.56028900		88.972
50	156.823775545	1.072372528				79.549
51	118.692607648	80.006000000	SIC2	1.56028900		72.749
52	0.000000000	8.436241391	Immersion	1.560000000		19.439
53	0.000000000	0.000000000				11.000

Table 2

ASPHERIC CONSTANTS

SURFACE NO. 4

K	0.0000
C1	2.13047921e-007
C2	-3.57933301e-011
C3	2.93263063e-015
C4	-4.61461071e-019
C5	2.76061570e-023
C6	1.62740830e-027
C7	-3.43732853e-031
C8	0.00000000e-000
C9	0.00000000e+000

SURFACE NO. 44

K	0.0000
C1	-5.18910040e-009
C2	3.51025484e-013
C3	-5.47716488e-016
C4	4.43561455e-023
C5	3.42844064e-028
C6	-1.97724021e-032
C7	2.22456117e-037
C8	0.00000000e+000
C9	0.00000000e+000

SURFACE NO. 6

K	0.0000
C1	-1.14265623e-007
C2	2.02166625e-011
C3	-1.76403105e-015
C4	2.36305340e-019
C5	-2.55314839e-023
C6	1.35459868e-027
C7	-2.70730236e-032
C8	0.00000000e+000
C9	0.00000000e+000

SURFACE NO. 25

K	0.0000
C1	-9.78914413e-008
C2	-4.33166283e-012
C3	-8.01001563e-017
C4	-1.31611936e-019
C5	6.54375176e-023
C6	-1.37293557e-026
C7	1.58764578e-030
C8	0.00000000e+000
C9	0.00000000e+000

SURFACE NO. 29

K	0.0000
C1	2.99497807e-008
C2	-3.16131943e-012
C3	-8.61008384e-017
C4	2.05647555e-020
C5	-2.56167018e-024
C6	1.74321022e-028
C7	-7.59802684e-033
C8	0.00000000e+000
C9	0.00000000e+000

SURFACE NO. 34

K	0.0000
C1	-5.83593306e-009
C2	-4.08253893e-015
C3	-3.40928951e-015
C4	1.36466423e-022
C5	-1.03090955e-026
C6	4.02018916e-031
C7	-9.89542759e-036
C8	0.00000000e+000
C9	0.00000000e+000

Table 3

SURFACE	RADI	THICKNESSES	LENS	REFRACTIVE INDEX ???.?? mm	1/2 FREE DIAMETER
0	0.000000000	21.980160000	L710	0.99998200	55.000
1	0.000000000	6.220362492	L710	0.99998200	59.574
2	-603.070624671	5.913063455	SIO2HL	1.56028900	60.690
3	280.916333783	13.100217803	HE193	0.99971200	64.385
4	-461.660531347AS	6.000000000	SIO2HL	1.56028900	65.798
5	681.261406487	25.180513824	HE193	0.99971200	70.487
6	421.796712825AS	13.410528997	S1C3HL	1.56028900	69.920
7	306.236502978	23.641056301	HE193	0.99971200	95.293
8	-881.743075986	64.144962259	SJ02HL	1.56028900	97.777
9	-397.616226767	1.032715830	HE193	0.99971200	123.195
10	-1049.995266570	23.472283137	SIO2HL	1.56028900	130.947
11	-286.549348161	2.251083976	HE193	0.99971200	136.447
12	-655.273684770	52.089256568	SIO2HL	1.56028900	143.894
13	-205.267390137	1.028491553	HE193	0.99971200	146.415
14	-565.795559961	15.822681399	SIO2HL	1.56028900	145.408
15	-410.848668817	1.000000613	HE193	0.99971200	146.045
16	809.207497255	27.599045382	SIO2HL	1.56028900	142.434
17	-599.260287529AS	1.000000015	HE193	0.99971200	141.453
18	136.304267826	62.52385200	SIO2HL	1.56028900	113.454
19	157.516637917	1.000000000	HE193	0.99971200	101.084
20	126.013978931	24.051407776	SIO2HL	1.56028900	96.007
21	157.519818688	23.554259229	HE193	0.99971200	84.914
22	795.455608357	9.035828932	SIO2HL	1.56028900	82.369
23	78.910295718	18.235914318	HE193	0.99971200	63.551
24	-647.136797738	5.060000184	SIO2HL	1.56028900	63.056
25	148.158813477AS	12.440106724	HE193	0.99971200	61.484
26	-157.858636028	5.960377452	SIO2HL	1.56028900	62.472
27	1367.448704100	41.067582498	HE193	0.99971200	66.716
28	-87.255013445	0.475217865	SIO2HL	1.56028900	68.713
29	-396.760639119AS	6.472661890	HE193	0.99971200	80.202
30	-317.095597644	34.30021646	SIO2HL	1.56028900	90.935
31	-136.816156215	1.956487291	HE193	0.99971200	96.054
32	-384.621022314	18.250851268	SIO2HL	1.56028900	107.862
33	-158.063116797	1.000000006	HE193	0.99971200	111.057
34	807.690134076AS	41.496271568	SIO2HL	1.56028900	117.585
35	-280.885153902	25.354810908	HE193	0.99971200	117.901
36	-166.502630134	5.238823967	SIO2HL	1.56028900	117.263
37	988.468038668	6.681211723	HE193	0.99971200	131.802
38	1106.563200370	44.085972378	SIO2HL	1.56028900	134.587
39	-353.437766566	1.000000005	HE193	0.99971200	136.483
40	445.824457242	52.624318854	SIO2HL	1.56028900	142.739
41	-460.556866224AS	26.156809880	HE193	0.99971200	142.372
42	-248.318425801	36.706472160	SIO2HL	1.56028900	141.622
43	-340.049722714AS	16.312593082	HE193	0.99971200	146.673
44	0.000000000	12.526710616	HE193	0.99971200	142.237
45	1036.963505660	42.907366802	SIO2HL	1.56028900	142.523
46	-417.465602639	1.875432853	HE193	0.99971200	142.184
47	189.031074062	41.889218814	SIO2HL	1.56028900	121.251
48	698.095906560AS	1.076370948	HE193	0.99971200	117.434
49	109.988479121	24.053123871	SIO2HL	1.56028900	91.356
50	167.347263939	1.034746212	HE193	0.99971200	84.177
51	123.915863411	79.999373259	SIO2HL	1.56028900	77.713
52	0.000000000	10.366030727	JMMERS	1.370000000	25.089
53	0.000000000	0.000000000		1.000000000	11.000

Table 4

ASPHERIC CONSTANTS

SURFACE NO. 4		SURFACE NO. 34	
K	0.0000	K	0.0000
C1	2.26522214e-007	C1	-4.23637017e-009
C2	-3.59236651e-011	C2	-3.29710303e-014
C3	2.92133725e-015	C3	-3.52756803e-018
C4	-3.77696224e-019	C4	-4.13266120e-023
C5	7.96388858e-024	C5	-2.16653680e-027
C6	3.51988385e-027	C6	2.27691141e-031
C7	-4.54711324e-031	C7	-8.70596013e-036
C8	0.00000000e+000	C8	0.00000000e+000
C9	0.00000000e+000	C9	0.00000000e+000
SURFACE NO. 6		SURFACE NO. 41	
K	0.0000	K	0.0000
C1	-1.19063117e-007	C1	3.45855942e-009
C2	1.94132266e-011	C2	5.47566277e-014
C3	-1.61962009e-015	C3	-3.85610770e-018
C4	2.25193097e-019	C4	2.74041138e-023
C5	-2.25566558e-023	C5	1.86632362e-027
C6	1.19237134e-027	C6	-3.44742394e-032
C7	-2.51584924e-032	C7	3.29571792e-038
C8	0.00000000e+000	C8	0.00000000e+000
C9	0.00000000e+000	C9	0.00000000e+000
SURFACE NO. 17		SURFACE NO. 43	
K	0.0000	K	0.0000
C1	1.74375723e-011	C1	-3.55873802e-010
C2	-2.04129734e-014	C2	9.63322458e-014
C3	7.67666306e-015	C3	-7.64415866e-019
C4	-1.93715606e-022	C4	2.00153471e-023
C5	1.92834024e-027	C5	-1.98329358e-027
C6	-7.02565837e-032	C6	5.52524526e-032
C7	1.14576119e-036	C7	-4.80876507e-037
C8	0.00000000e+000	C8	0.00000000e+000
C9	0.00000000e+000	C9	0.00000000e+000
SURFACE NO. 25		SURFACE NO. 46	
K	0.0000	K	0.0000
C1	-6.29705361e-008	C1	-2.25289484e-009
C2	-3.25537639e-012	C2	2.62711822e-013
C3	-2.93013408e-016	C3	3.12883195e-018
C4	-9.17751598e-020	C4	-2.96009757e-022
C5	4.34261555e-023	C5	1.93969203e-026
C6	-1.01961896e-026	C6	-7.02702044e-031
C7	1.42841266e-030	C7	1.40329412e-035
C8	0.00000000e+000	C8	0.00000000e+000
C9	0.00002000e+000	C9	0.00000000e+000
SURFACE NO. 29			
K	0.0000		
C1	3.01669174e-009		
C2	-4.16186211e-012		
C3	-2.10017649e-017		
C4	1.39690846e-020		
C5	-1.51163159e-024		
C6	6.56920089e-029		
C7	-3.15414270e-033		
C8	0.00000000e+000		
C9	0.00000000e+000		

Table 5

SURFACE	RADII	THICKNESSES	LENSES	REFRACTIVE INDEX	1/2 FREE DIAMETER
				???.?? mm	
0	0.000000000	21.580160000	L710	1.000000000	55.000
1	0.000000000	5.521159992	L710	1.000000000	59.973
2	-653.380153342	10.75637537	CAF2HL	1.55848720	60.652
3	234.066815376	14.152447066	HE193	1.000000000	64.672
4	-541.443785623AS	8.065016137	CAF2HL	1.55848720	66.216
5	805.087192810	22.060952617	HE193	1.000000000	70.663
6	637.617712375AS	16.925405960	CAF2HL	1.55848720	88.269
7	315.047932823	22.112216303	HE193	1.000000000	94.661
8	-1055.166104073	68.241607282	CAF2HL	1.55848720	97.341
9	-440.417777767	1.950157109	HE193	1.000000000	124.495
10	-833.235756565	45.202958015	CAF2HL	1.55848720	130.520
11	-248.097167968	6.567867993	HE193	1.000000000	136.785
12	-667.629333065	58.5277118374	CAF2HL	1.55848720	147.021
13	-230.265801432	1.000000000	HE193	1.000000000	152.069
14	-635.989091493	52.689533957	CAF2HL	1.55848720	151.782
15	-420.897960530	1.000000000	HE193	1.000000000	155.231
16	682.574050518	42.565465696	CAF2HL	1.55848720	150.819
17	-650.602325928AS	1.000000000	HE193	1.000000000	149.697
18	145.905393739	39.312156678	CAF2HL	1.55848720	117.562
19	170.361035751	1.000000000	HE193	1.000000000	106.663
20	127.366697165	53.064765940	CAF2HL	1.55848720	99.558
21	149.757517850	27.658696477	HE193	1.000000000	88.267
22	893.404652749	8.000000000	CAF2HL	1.55848720	85.687
23	95.474739306	42.082501866	HE193	1.000000000	67.021
24	-556.412618267	6.000000000	CAF2HL	1.55848720	65.854
25	113.887772525AS	36.095767773	HE193	1.000000000	63.605
26	-202.032636775	8.000000000	CAF2HL	1.55848720	64.919
27	-1368.827225050	39.670258843	HE193	1.000000000	68.993
28	-87.722719327	6.1509219605	CAF2HL	1.55848720	70.057
29	-341.867554503AS	7.243142706	HE193	1.000000000	89.680
30	-270.353733321	34.012062471	CAF2HL	1.55848720	92.272
31	-131.525576131	1.000000000	HE193	1.000000000	97.490
32	-356.379287278	37.218470508	CAF2HL	1.55848720	109.741
33	-160.4867325217	1.000000000	HE193	1.000000000	113.010
34	726.417351927AS	44.411516365	CAF2HL	1.55848720	121.086
35	-285.951760863	26.777077267	HE193	1.000000000	121.404
36	-169.413078236	6.000000000	CAF2HL	1.55848720	120.698
37	1233.439177430	5.704973599	HE193	1.000000000	135.515
38	1968.954811160	42.925033480	CAF2HL	1.55848720	136.862
39	-334.436426428	1.000000000	HE193	1.000000000	136.795
40	448.482885926	53.5152735929	CAF2HL	1.55848720	145.983
41	-481.776223591AS	38.664604302	HE193	1.000000000	145.641
42	-257.207339099	39.651511432	CAF2HL	1.55848720	141.395
43	-352.351244424AS	6.074724759	HE193	1.000000000	146.219
44	0.000000000	8.135112666	HE193	1.000000000	142.806
45	1571.538613070	41.393617207	CAF2HL	1.55848720	143.060
46	-395.530196939	4.955626551	HE193	1.000000000	142.883
47	185.59455401	44.893603417	CAF2HL	1.55848720	122.056
48	737.460220721AS	1.254530428	HE193	1.000000000	117.739
49	113.971025152	34.166140572	CAF2HL	1.55848720	91.975
50	186.560340242	1.000000000	HE193	1.000000000	85.629
51	124.935012572	92.227372544	CAF2HL	1.55848720	76.952
52	0.000000000	0.050000026	IMMERS	1.370000000	11.068
53	0.000000000	0.000000000		1.000000000	11.000

Table 6

ASPHERIC CONSTANTS

SURFACE NO.	4	SURFACE NO.	34
K	7.3905	K	1.5440
C1	2.19490389e-007	C1	-3.43267330e-009
C2	-3.16478613e-011	C2	-1.34450662e-014
C3	2.6569241e-015	C3	-2.25266384e-016
C4	-3.54256715e-019	C4	9.7572967e-023
C5	1.30325174e-023	C5	-1.35202712e-026
C6	2.26447806e-027	C6	8.00518329e-031
C7	-2.5478129e-031	C7	-2.65068179e-035
C8	0.00000000e+000	C8	0.00000000e+000
C9	0.00000000e+000	C9	0.00000000e+000
SURFACE NO.	6	SURFACE NO.	41
K	0.5253	K	0.0872
C1	-1.14294859e-007	C1	3.26909609e-009
C2	1.87842386e-011	C2	7.76009100e-014
C3	-1.75164086e-015	C3	-3.82550397e-018
C4	2.34304280e-019	C4	2.28007850e-023
C5	-2.31194495e-023	C5	-2.34153651e-028
C6	1.12536497e-027	C6	1.34376006e-032
C7	-2.03074756e-032	C7	-1.01621512e-036
C8	0.00000000e+000	C8	0.00000000e+000
C9	0.00000000e+000	C9	0.00000000e+000
SURFACE NO.	17	SURFACE NO.	43
K	0.7878	K	0.0312
C1	-3.05430457e-010	C1	-4.99667832e-010
C2	-4.89773138e-014	C2	1.15316140e-013
C3	1.06523190e-016	C3	-1.1640795e-018
C4	-1.47516554e-023	C4	7.05365641e-023
C5	1.34257246e-027	C5	-2.43649494e-027
C6	-5.23906249e-032	C6	6.83361566e-032
C7	8.17069597e-037	C7	-6.25588420e-037
C8	0.00000000e+000	C8	0.00000000e+000
C9	0.00000000e+000	C9	0.00000000e+000
SURFACE NO.	25	SURFACE NO.	45
K	0.0012	K	-1.8716
C1	-6.90163181e-008	C1	-4.03414746e-009
C2	-2.08603493e-012	C2	1.94301708e-013
C3	-3.48956288e-016	C3	4.07775084e-018
C4	-3.58451964e-020	C4	-4.70574709e-022
C5	2.16254654e-023	C5	2.42642656e-026
C6	-3.58801026e-027	C6	-8.38949812e-031
C7	6.6000225e-031	C7	1.38185311e-035
C8	0.00000000e+000	C8	0.00000000e+000
C9	0.00000000e+000	C9	0.00000000e+000
SURFACE NO.	29		
K	-0.0334		
C1	3.02609727e-005		
C2	-3.89225347e-012		
C3	-2.00302538e-017		
C4	1.38850354e-020		
C5	-1.75136022e-024		
C6	5.45164389e-029		
C7	-4.34831621e-033		
C8	0.00000000e+000		
C9	0.00000000e+000		

Table 7

SURFACE	RADII	THICKNESSES	LENSES	REFRACTIVE INDEX	1/2 FREE DIAMETER
				157.6 nm	
0	0.000000000	21.980160000			55.000
1	0.000261400	5.696922030			55.974
2	-683.677052960	0.000016965	CAF2HL	1.55848720	60.653
3	241.845116194	13.452175419			64.060
4	-561.327374516AS	8.000000000	CAF2HL	1.55848720	65.556
5	695.454774317	23.262413511			69.867
6	400.792577467AS	11.762291230	CAF2HL	1.55848720	88.232
7	293.254619517	22.305108600			92.835
8	-1055.362319550	71.454892862	CAF2HL	1.55848720	95.242
9	-483.111722442	2.387528569			124.161
10	-967.495111648	48.847817148	CAF2HL	1.55848720	130.362
11	-225.898512938	5.659224997			136.444
12	-579.940954244	54.879651202	CAF2HL	1.55848720	145.324
13	-221.617621858	1.000000000			149.602
14	-775.372221125	15.081823940	CAF2HL	1.55848720	147.807
15	-525.919666317	1.000000000			148.157
16	660.302511324	38.720317303	CAF2HL	1.55848720	144.440
17	-732.46791129AS	1.000000000			143.303
18	147.955956945	38.941140120	CAF2HL	1.55848720	116.315
19	174.554421407	1.000000000			105.360
20	118.333525649	33.404122786	CAF2HL	1.55848720	96.491
21	140.21612698	28.013496674			85.972
22	788.027935344	8.657239650	CAF2HL	1.55848720	83.494
23	03.038132631	41.178404325			65.374
24	-597.396361251	8.000000000	CAF2HL	1.55848720	64.284
25	136.95601e017AS	31.536496066			62.327
26	-200.199232002	8.000000000	CAF2HL	1.55848720	63.210
27	1650.730497660	63.442178500			66.558
28	-86.362069271	8.216360232	CAF2HL	1.55848720	69.385
29	-360.179451575AS	2.567422592			89.255
30	-280.601605532	34.872981631	CAF2HL	1.55848720	92.027
31	-132.713344295	1.004709559			97.215
32	-361.6621418157	37.722657596	CAF2HL	1.55848720	109.325
33	-159.165877620	1.000000000			112.571
34	750.946018427AS	43.541363913	CAF2HL	1.55848720	120.144
35	-265.80C553705	25.930047160			120.440
36	-169.581349559	8.030377840	CAF2HL	1.55848720	119.789
37	1077.110465570	5.6629859689			134.105
38	1605.653205560	43.332820801	CAF2HL	1.55848720	135.539
39	-333.794563037	1.000000000			137.425
40	448.582489713	52.027765048	CAF2HL	1.55848720	144.043
41	-487.266144069AS	37.362834300			143.681
42	-256.680121302	40.279714930	CAF2HL	1.55848720	139.818
43	-353.759C21671AS	7.564240061			144.656
44	0.000000300	10.832272687			141.334
45	1499.148500020	42.690870531	CAF2HL	1.55848720	141.660
46	-394.545474104	2.390581943			141.445
47	168.580735298	63.317430646	CAF2HL	1.55848720	121.630
48	731.593986095AS	1.000000000			117.959
49	114.385993339	38.526813476	CAF2HL	1.55848720	92.421
50	184.018615075	1.000000000			85.485
51	123.357013160	93.333950169	CAF2HL	1.55848720	77.332
52	0.000000000	0.050000000	Immersion	1.370000000	11.068
53	0.000000000	0.000000000			11.000

Table 8

ASPHERIC CONSTANTS

SURFACE NO. 4

K	2.0014
C1	2.24631581e-007
C2	-3.32117029e-011
C3	2.75311747e-015
C4	-3.76346953e-019
C5	1.61561324e-023
C6	2.15579277e-027
C7	-2.81811737e-031
C8	0.00000000e+000
C9	0.00000000e+000

SURFACE NO. 6

K	1.5259
C1	-1.12174954e-007
C2	1.85334618e-011
C3	-1.79334960e-015
C4	2.22576675e-019
C5	-2.32368876e-023
C6	1.17478944e-027
C7	-2.27644098e-032
C8	0.00000000e+000
C9	0.00000000e+000

SURFACE NO. 17

K	1.0236
C1	-4.04184504e-010
C2	-5.52221210e-014
C3	1.07792613e-018
C4	-9.68577933e-024
C5	1.93184487e-027
C6	-7.57233584e-032
C7	1.33745628e-036
C8	0.00000000e+000
C9	0.00000000e+000

SURFACE NO. 25

K	0.0056
C1	-6.73576580e-002
C2	-2.60111173e-012
C3	-4.29261635e-016
C4	-8.53651144e-020
C5	3.61021613e-023
C6	-7.30626628e-027
C7	1.01531199e-030
C8	0.00000000e+000
C9	0.00000000e+000

SURFACE NO. 49

K	-0.2758
C1	3.11035863e-008
C2	-4.09777758e-012
C3	-6.25551384e-016
C4	1.47181039e-020
C5	-1.67735576e-024
C6	7.46972419e-028
C7	-2.04782511e-032
C8	0.00000000e+000
C9	0.01400000e+000

SURFACE NO. 34

K	1.5943
C1	-3.41675063e-005
C2	-1.06207572e-014
C3	-2.75870107e-010
C4	1.25443795e-022
C5	-1.53842992e-026
C6	9.81335165e-031
C7	-2.88557010e-035
C8	0.00000000e+000
C9	0.00000000e+000

SURFACE NO. 41

K	0.1099
C1	3.24105758e-009
C2	7.37348572e-014
C3	-1.58460435e-018
C4	2.55537441e-023
C5	-1.78466202e-020
C6	1.62622698e-032
C7	-1.16103266e-036
C8	0.00000000e+000
C9	0.00000000e+000

SURFACE NO. 43

K	0.0331
C1	-4.94661761e-010
C2	1.05503739e-013
C3	-1.45124635e-016
C4	6.84609756e-023
C5	-2.60450711e-027
C6	7.57276741e-032
C7	-7.11474674e-037
C8	0.00000000e+000
C9	0.00000000e+000

SURFACE NO. 48

K	-1.6262
C1	-4.00081230e-005
C2	1.92491101e-013
C3	3.74576193e-018
C4	-4.50566284e-022
C5	2.41249474e-026
C6	-8.61661412e-031
C7	1.44171993e-035
C8	0.00000000e+000
C9	0.00000000e+000

Table 9

SURFACE	RADIUS	THICKNESSES	LENSES	REFRACTIVE INDEX 193.168 nm	1/2 FREE DIAMETER
0	0.0000160000	21.980160000		1.000000000	56.060
1	0.0000000000	3.21688384	L710	0.99998200	61.157
2	-7758.072575491	6.000000000	SIO2HL	1.56028900	61.896
3	355.729181657	7.529172915	HE192	0.99971200	63.992
4	1890.30584462AS	6.000000000	SIO2HL	1.56028900	65.078
5	268.211281606	15.157771412	HE193	0.99971200	68.460
6	3183.174654849AS	8.000000000	SIO2HL	1.56028900	72.301
7	542.737427521	25.226019508	HE193	0.99971200	76.281
8	-190.186655474	56.302346531	SIO2HL	1.56028900	78.244
9	-200.572551645	1.000000000	HE193	0.99971200	102.934
10	-1181.735114120	41.616051168	SIO2HL	1.56028900	116.315
11	-200.599701129	1.000000000	HE193	0.99971200	119.335
12	-345.801617036	34.756009233	SIO2HL	1.56028900	122.895
13	-183.035540027	1.000000000	HE193	0.99971200	125.001
14	468.896324219	28.888366130	SIO2HL	1.56028900	119.583
15	-1579.320375454AS	1.000000000	HE193	0.99971200	118.610
16	130.622577421	25.607493426	SIO2HL	1.56028900	101.535
17	167.643755366	1.000000000	HE193	0.99971200	96.903
18	109.515011627	33.485629573	SIO2HL	1.56028900	88.871
19	135.857752039	27.284751341	HE193	0.99971200	79.284
20	8434.056206242	6.000000000	SIO2HL	1.56028900	76.872
21	75.280373304	30.508120723	HE193	0.99971200	60.167
22	712.917049547	6.000000000	SIO2HL	1.56028900	59.980
23	137.647950319AS	41.376149828	HE193	0.99971200	58.756
24	-120.168111858	8.000000000	SIO2HL	1.56028900	60.070
25	-335.689956101	26.955101014	HE193	0.99971200	64.725
26	-86.294324443	8.405631441	SIO2HL	1.56028900	65.622
27	-401.221576575AS	6.791819241	HE193	0.99971200	82.386
28	-295.528316034	33.017957091	SIO2HL	1.56028900	84.761
29	-156.211920654	1.000000000	HE193	0.99971200	93.276
30	-266.579127336	33.049041389	SIO2HL	1.56028900	99.716
31	-143.116314621	1.000000000	HE193	0.99971200	103.445
32	472.6935961019AS	41.687451272	SIO2HL	1.56028900	115.709
33	-346.217411641	22.889302349	HE193	0.99971200	116.094
34	-187.601096847	12.645469238	SIO2HL	1.56028900	115.710
35	-359.852656461	1.000000000	HE193	0.99971200	121.777
36	722.017664882	60.459509481	SIO2HL	1.56028900	125.218
37	-1816.432711561AS	24.260456335	HE193	0.99971200	125.322
38	2199.260274610	24.178147653	SIO2HL	1.56028900	124.815
39	-1512.556711535	6.000000000	HE193	0.99971200	124.440
40	0.000000000	14.309578556	HE193	0.99971200	123.088
41	1738.196396601	35.559449287	SIO2HL	1.56028900	124.310
42	-429.627570104AS	1.000000000	HE193	0.99971200	124.575
43	179.589162742	55.687793355	SIO2HL	1.56028900	115.507
44	589.027987143AS	10.530033379	HE193	0.99971200	105.186
45	136.621156861	53.097751469	SIO2HL	1.56028900	89.320
46	137.713631620	1.000000000	HE192	0.99971200	67.001
47	93.226477153	90.565495277	SIO2HL	1.56028900	62.139
48	0.000000000	1.0000000545	IMMERS	1.56000000	14.735
49	0.000000000	0.000000000		1.000000000	14.020

Table 10

ASPHERIC CONSTANTS

SURFACE NO. 6

K	0.0000
C1	2.01531001e-007
C2	-3.99703415e-011
C3	2.76850090e-015
C4	-4.54867122e-019
C5	-5.66904777e-024
C6	5.03662466e-027
C7	-4.52060360e-031
C8	0.00000000e+000
C9	0.00000000e+000

SURFACE NO. 6

K	0.0000
C1	-1.16706261e-007
C2	2.00348321e-011
C3	-1.51130378e-015
C4	3.05660555e-019
C5	-1.76658953e-023
C6	3.15835636e-027
C7	-4.23595936e-031
C8	0.00000000e+000
C9	0.00000000e+000

SURFACE NO. 15

K	0.0000
C1	-9.37524970e-010
C2	-2.58161066e-013
C3	-5.12206559e-018
C4	1.60598481e-022
C5	3.60535800e-027
C6	3.85878819e-031
C7	-3.50150744e-037
C8	0.00000000e+000
C9	0.00000000e+000

SURFACE NO. 23

K	0.0000
C1	-9.05676602e-008
C2	-7.64727914e-013
C3	-9.31E67049e-016
C4	9.20035750e-020
C5	-9.15433014e-023
C6	1.32736186e-026
C7	-9.23872382e-031
C8	0.00000000e+000
C9	0.00000000e+000

SURFACE NO. 27

K	0.0000
C1	2.51519254e-008
C2	-4.37829106e-012
C3	2.66587306e-017
C4	1.45024261e-020
C5	-1.31152094e-024
C6	1.02657156e-030
C7	-5.71174949e-034
C8	0.00000000e+000
C9	0.50770000e+001

SURFACE NO. 32

K	0.0000
C1	-2.59166418e-009
C2	-6.93760219e-014
C3	-4.25486946e-018
C4	3.13097668e-022
C5	-1.87333640e-026
C6	1.28572875e-030
C7	-3.94471730e-035
C8	0.00000000e+000
C9	0.00000000e+000

SURFACE NO. 37

K	0.0000
C1	3.92265908e-009
C2	5.90432031e-014
C3	-4.61273256e-018
C4	5.09437288e-023

Patent Claims

1. Refractive projection objective for projecting a pattern arranged in an object plane of the projection objective into an image plane of the projection objective with the aid of an immersion medium which is arranged between a last optical element of the projection objective and the image plane, comprising:
 - a first lens group (LG1), following the image plane, with a negative refracting power;
 - a second lens group (LG2), following the first lens group, with a positive refracting power;
 - a third lens group (LG3), following the second lens group, with a negative refracting power;
 - a fourth lens group (LG4), following the third lens group, with a positive refracting power;
 - a fifth lens group (LG5), following the fourth lens group, with a positive refracting power; and
 - a system aperture (5) which is arranged in the region of maximum beam diameter between the fourth and the fifth lens group.
2. Projection objective according to Claim 1, wherein the system aperture (5) lies between a plane of maximum beam diameter near the image and the image plane (3).
3. Projection objective according to Claim 1 or 2 which has an image-side numerical aperture $NA \geq 0.9$, the image-side numerical aperture preferably being at least $NA = 1.0$.
4. Projection objective according to one of the preceding claims, wherein the projection objective is adapted to an immersion medium (10) which has a refractive index of $n > 1.3$ at the operating wavelength.

5. Projection objective according to one of the preceding claims, wherein the projection objective has an image-side working distance of between approximately 10 μm and approximately 200 μm , in particular between approximately 20 μm and approximately 100 μm .
6. Projection objective according to one of the preceding claims, wherein a ratio between the focal length of the fourth lens group (LG4) and the focal length of the fifth lens group (LG5) is between approximately 0.9 and approximately 1.1.
7. Projection objective according to one of the preceding claims, wherein a ratio of the magnitudes of the focal lengths of the first lens group (LG1) and the fifth lens group (LG5) is between approximately 0.7 and approximately 1.3, in particular between approximately 0.9 and approximately 1.1.
8. Projection objective according to one of the preceding claims, wherein a ratio between the overall length of the projection objective and the focal length of the fifth lens group (LG5) is greater than five, preferably greater than six, in particular greater than eight.
9. Projection objective according to one of the preceding claims, wherein the first lens group (LG1) includes at least one aspheric surface, two aspheric surfaces preferably being provided in the first lens group.
10. Projection objective according to one of the preceding claims, wherein at least one aspheric surface is provided in the third lens group (LG3), two aspheric surfaces preferably being provided.
11. Projection objective according to one of the preceding claims, wherein at least one aspheric surface is arranged in the first lens group,

and/or wherein not more than nine aspheric surfaces are provided, less than seven aspheric surfaces preferably being provided.

12. Projection objective according to one of the preceding claims, wherein at least one meniscus lens (13), convex relative to the object plane, with a negative refracting power is arranged in the near zone of the object plane (2), in particular inside the first lens group (LG1).

13. Projection objective according to one of the preceding claims, wherein the second lens group has at least four, preferably at least five or six consecutive lenses (14 to 20) with a positive refracting power.

14. Projection objective according to one of the preceding claims, wherein the second lens group (LG2) has at least one, preferably a plurality of meniscus lenses (14, 15, 16, 17), concave relative to the object plane, with a positive refracting power on an entry side facing the object plane (2), and/or wherein the second lens group has at least one, preferably a plurality of meniscus lenses (19, 20), convex relative to the object plane, with a positive refracting power on the exit side facing the image plane.

15. Projection objective according to one of the preceding claims, wherein the second lens group (LG2) in this sequence has at least one meniscus lens (14, 15, 16, 17), concave relative to the object plane, with a positive refracting power, a biconvex positive lens (18) and at least one meniscus lens (19, 20), concave relative to the image plane, with a positive refracting power.

16. Projection objective according to one of the preceding claims, wherein the third lens group (LG3) has only lenses (21, 22, 23, 24) with a negative refracting power.

17. Projection objective according to one of the preceding claims, wherein, with reference to a plane (9) of symmetry lying inside the third lens group (LG3), the third lens group is of substantially symmetrical construction, and/or wherein two oppositely curved, concave surfaces directly opposed to one another in the third lens group (LG3) and are surrounded by two concave surfaces which are concave relative to one another.
18. Projection objective according to one of the preceding claims, wherein an exit region, facing the third lens group (LG3), of the second lens group (LG2), and an entry region, following the third lens group, of the fourth lens group (LG4) are constructed substantially symmetrically relative to a plane (9) of symmetry lying inside the third lens group.
19. Projection objective according to one of the preceding claims, wherein the fourth lens group (LG4) has at least one doublet (27, 28, 29, 30) with a biconvex positive lens (27, 29) and a downstream negative meniscus lens (28, 30) with lens surfaces which are concave towards the object, at least two doublets preferably being provided.
20. Projection objective according to one of the preceding claims, wherein in an object-side entry region the fourth lens group (LG4) has at least one meniscus lens (25, 26), concave relative to the object plane (2), with a positive refracting power, a plurality of such meniscus lenses preferably being provided consecutively.
21. Projection objective according to one of the preceding claims, wherein the sine of the maximum incidence angle of the radiation impinging on the optical surfaces is less than 90%, in particular less than 85% of the image-side numerical aperture.

22. Projection objective according to one of the preceding claims, wherein the fifth lens group (LG5) has exclusively lenses with a positive refracting power.
23. Projection objective according to one of the preceding claims, wherein the fifth lens group has at least four positive lenses (31 to 35).
24. Projection objective according to one of the preceding claims, wherein the fifth lens group (LG5) has at least one meniscus lens (33, 34) with a positive refracting power and lens surfaces concave towards the image.
25. Projection objective according to one of the preceding claims, wherein as last optical element the fifth lens group (LG5) has a plano-convex lens (35) which preferably has a spherical entry surface and a substantially flat exit surface.
26. Projection objective according to Claim 25, wherein the plano-convex lens (35) is constructed in a nonhemispherical fashion.
27. Projection objective according to one of the preceding claims, wherein all the lenses consist of the same material, use preferably being made of synthetic quartz glass as lens material for a 193 nm operating wavelength, and/or of calcium fluoride as lens material for a 157 nm wavelength.
28. Projection objective according to one of the preceding claims which is a single-waist system with a belly (6) near the object, a belly (8) remote from the object and a waist (7) therebetween.
29. Projection objective according to one of the preceding claims, wherein the image field diameter is more than 10 mm, in particular more

than 20 mm and/or wherein the image field diameter is more than 1.0%, in particular more than 1.5%, of the overall length.

30. Projection objective according to one of the preceding claims, wherein the light conductance is more than approximately 1%, in particular more than approximately 2% of the overall length.
31. Projection objective according to one of the preceding claims, wherein substantially more lenses are arranged upstream of the system aperture (5) than downstream of the system aperture, preferably at least four times as many.
32. Projection objective according to one of the preceding claims, wherein at least five lenses with a positive refracting power are arranged between the waist and the system aperture (5).
33. Projection objective according to one of the preceding claims, wherein a distance between the waist and the system aperture is at least 26% of the overall length, preferably more than 30% of the overall length.
34. Projection objective according to one of the preceding claims, wherein a maximum rim ray height is at least twice as large as the rim ray height at the location of the narrowest constriction.
35. Projection exposure machine for microlithography, characterized by a refractive projection objective (1, 1', 1'') in accordance with one of the preceding claims.
36. Method for producing semiconductor components and other finely structured structural elements, having the following steps:
providing a mask with a prescribed pattern;

illuminating the mask with ultraviolet light of a prescribed wavelength;
and
projecting an image of the pattern onto a photosensitive substrate,
arranged in the region of the image plane of a projection objective, with
the aid of a projection objective in accordance with one of the preceding
Claims 1 to 34;
an immersion medium arranged between a last optical surface of the
projection objective and the substrate being transilluminated during the
projection.

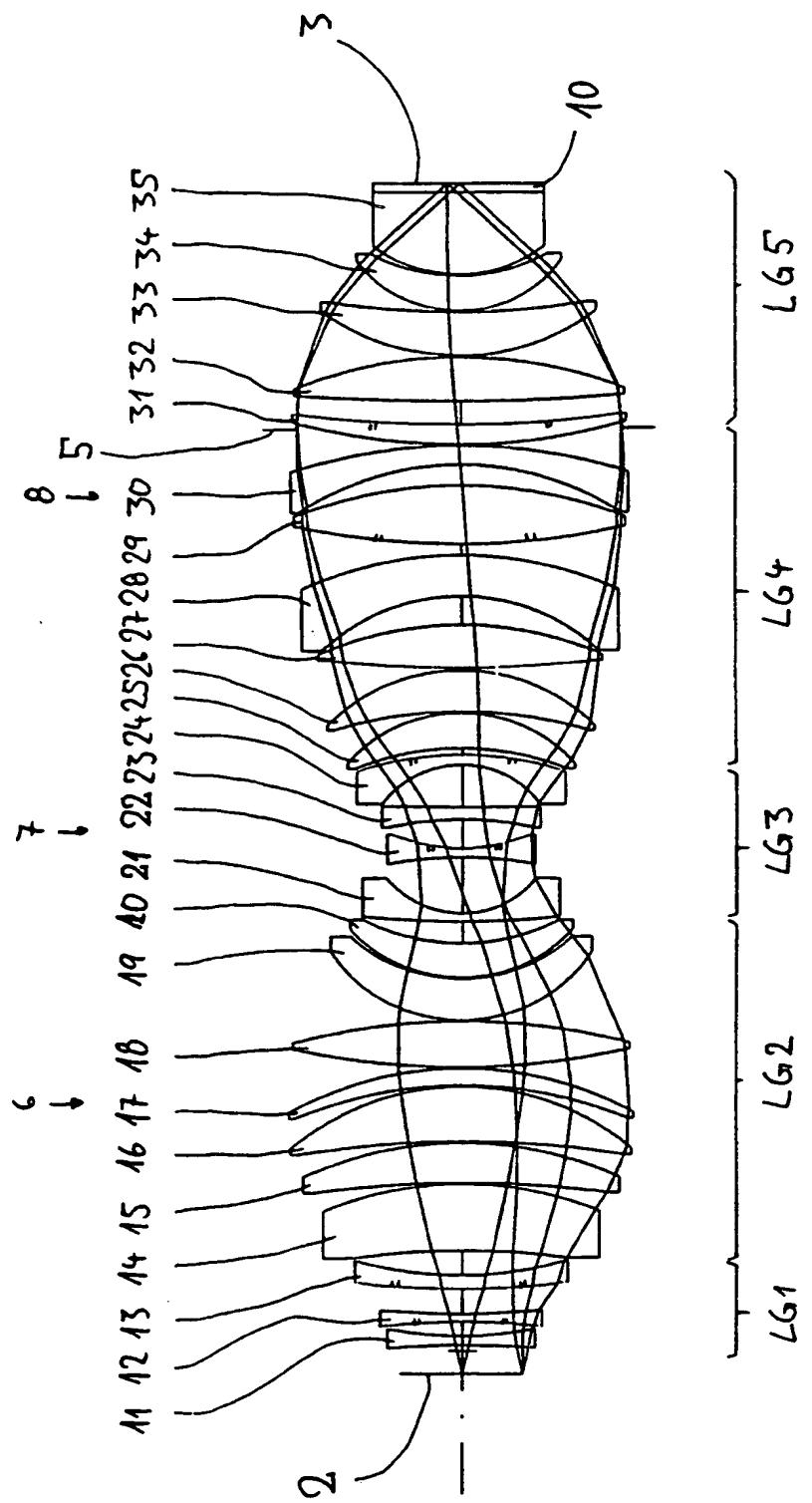


Fig. 1

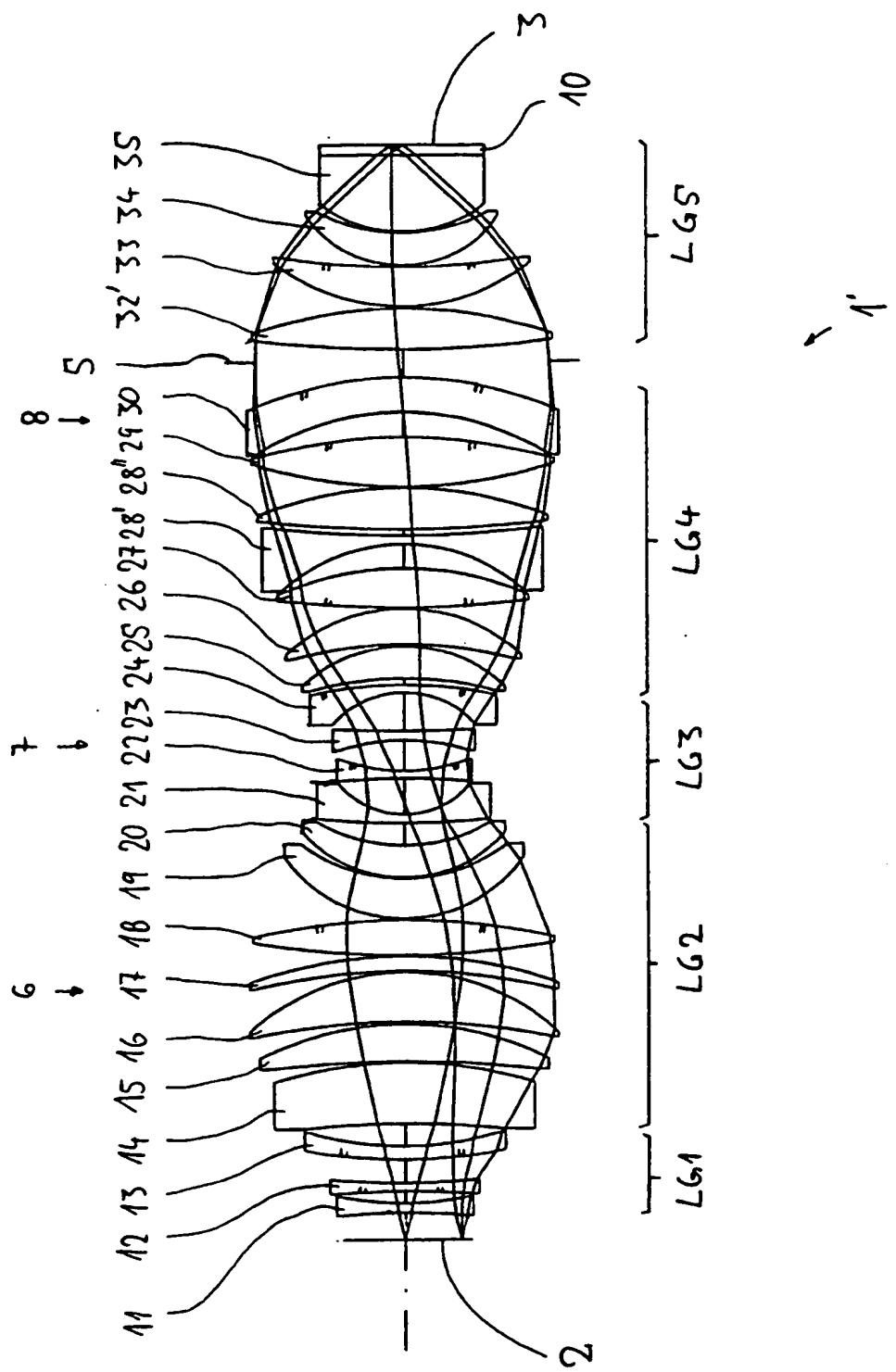


Fig. 2

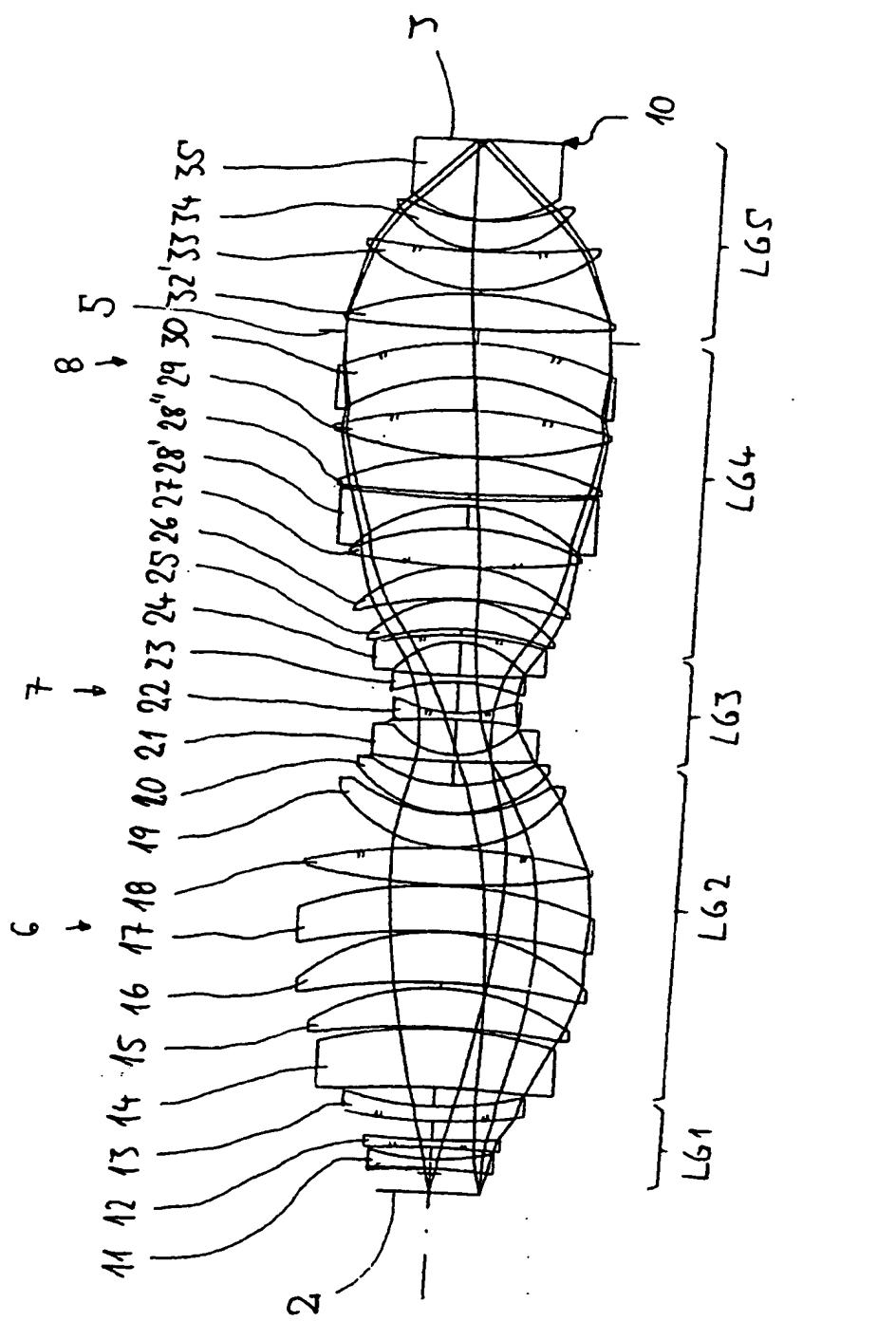


Fig. 3

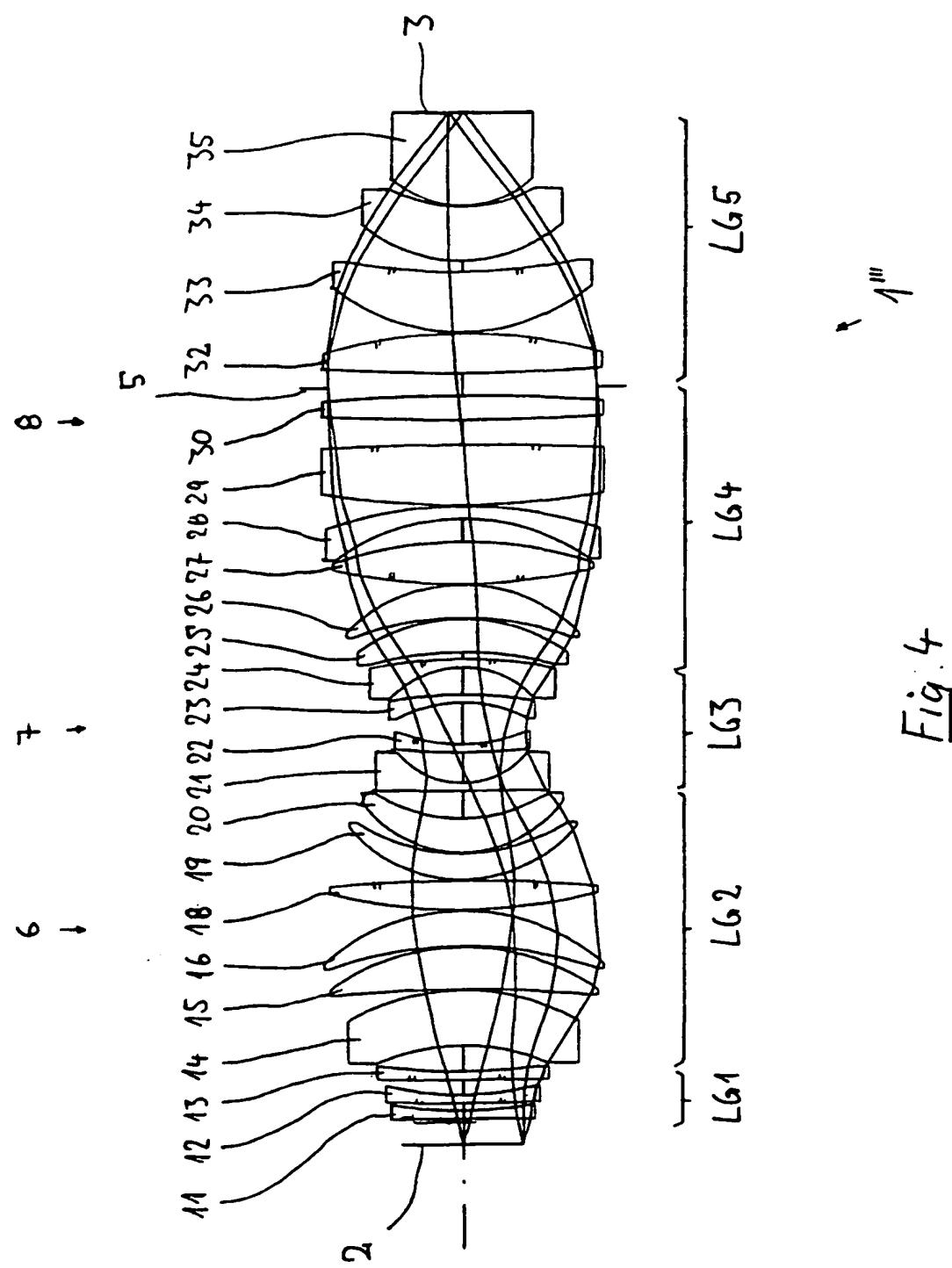


Fig. 4

INTERNATIONAL SEARCH REPORT

International Application No
PCT/EP 03/01954

A. CLASSIFICATION OF SUBJECT MATTER
IPC 7 603F7/20

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 7 603F

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the International search (name of data base and, where practical, search terms used)

EPO-Internal

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Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	EP 0 023 231 A (TABARELLI WERNER W DR) 4 February 1981 (1981-02-04) the whole document ----	1-36
Y	KAWATA H ET AL: "FABRICATION OF 0.2 MM FINE PATTERNS USING OPTICAL PROJECTION LITHOGRAPHY WITH AN OIL IMMERSION LENS" JAPANESE JOURNAL OF APPLIED PHYSICS, PUBLICATION OFFICE JAPANESE JOURNAL OF APPLIED PHYSICS. TOKYO, JP, vol. 31, no. 12B, PART 1, 1 December 1992 (1992-12-01), pages 4174-4177, XP000415418 ISSN: 0021-4922 abstract ----	1-36 -/-

Further documents are listed in the continuation of box C.

Patent family members are listed in annex.

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- *8* document member of the same patent family

Date of the actual completion of the International search	Date of mailing of the International search report
25 July 2003	01/08/2003
Name and mailing address of the ISA European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo nl, Fax: (+31-70) 340-3016	Authorized officer Daffner, M

INTERNATIONAL SEARCH REPORT

International Application No
PCT/EP 03/01954

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

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